

5

APPLICATION

FOR

UNITED STATES LETTERS PATENT

10

Be it known that we, Ionel Wechsler, residing at 10 Royce Road, Framingham,
Massachusetts 01701 and being a citizen of the United States, and Peter G. Marston,
residing at 28 Eastern Point Road, Gloucester, Massachusetts 01930 and being a citizen
of United States have invented a certain new and useful

METHOD AND SYSTEM FOR REMOVING SOLUTES FROM A FLUID USING
MAGNETICALLY CONDITIONED COAGULATION

of which the following is a specification:

15

Applicant: Wechsler *et al.*
For: METHOD AND SYSTEM FOR REMOVING CONTAMINANTS
FROM A FLUID USING MAGNETICALLY CONDITIONED
COAGULATION

5

FIELD OF INVENTION

This invention relates to removing contaminants from a fluid and more particularly, to a method and system for removing contaminants from a fluid using magnetically conditioned coagulation.

10

RELATED APPLICATIONS

This application is a continuation of U.S. Application Serial No. 10/225,872 filed on August 22, 2002, which is a continuation of U.S. Application Serial No. 09/873,625 filed on June 4, 2001, now abandoned, which is a continuation of U.S. Application Serial
15 No. 09/604,560 filed on June 27, 2000, now abandoned, which is a continuation of U.S. Application Serial No. 08/992,147 filed December 17, 1997, issued on August 5, 2000 as U.S. Patent No. 6,099,738.

BACKGROUND OF INVENTION

20

Many municipalities world-wide discharge their waste-water effluent into local waterways such as rivers, brooks, and ponds. Typically, however, the flow of such waterways is inadequate to carry away the residual nutrients, namely phosphates and nitrates, resulting in eutrophication of those waterways. That is, weeds and algae grow uncontrollably, due to the excessive nutrients, resulting in depletion of available oxygen
25 from the water. This results in killing the fish and amphibians which require the oxygen

for survival and ultimately turns the rivers and ponds into swamps, devoid of marine life.

Removing the nutrients (phosphates and nitrates) and other contaminants (cadmium, chromium, copper, lead, mercury, nickel, zinc, etc.) to safe levels is cost prohibitive. Guidelines proposed by the Environmental Protection Agency (EPA) and State Departments of the Environment to reduce the phosphate limits even further exacerbate the need for a cost effective, efficient method for removing the contaminant which will meet or exceed the existing and proposed EPA guidelines.

Recent studies have estimated the cost of nearing, not even achieving, the proposed EPA requirement for even modest sized facilities at tens of millions of dollars. Moreover, even then the existing technology cannot meet the requirements necessary to reverse eutrophication. Other attempts to meet the EPA requirement required a substantially high chemical consumption, and still failed to meet the EPA requirement.

Alternatives to meeting the EPA requirements include natural treatments, constructed wetlands, biological treatments and even relocation of treatment facility effluent, all of which are cost prohibitive. Magnetic filtration and separation systems have been attempted in the past. These systems provided magnetic filtration after coagulation, magnetic seeding, and flocculation. They did not incorporate magnetic preconditioning or magnetic field treatment of any kind. The only use of magnetic fields was in the devices used for filtration of the seeded, e.g. magnetic, flocs from the fluid. They did not recognize the benefit to coagulation of the magnetic field conditioning. Thus, they required comparatively large amounts of chemical reagents. Moreover, they did not achieve sufficient contaminant removal. See U.S. Patent No. 3,983,033, incorporated herein by this reference.

Magnetic treatment of water is disclosed in U.S. Patent No. 438,579 where a magnetic field is applied to water flowing through pipes in a closed boiler system in order to prevent minerals from depositing on the inside of the pipes by keeping the minerals suspended and flowing; the minerals are not collected and removed from the system.

Several other processing systems have been implemented to prevent scaling of precipitated minerals by applying a magnetic field transverse to a fluid to precipitate the minerals from solution. However, descriptions of these treatment specifically state that “treatment does not eliminate the hardness salts but alters them physically”. The precipitate is not collected. Prior art devices such as Moody, U.S. Patent No. 3,228,878, do not collect the contaminant but merely change the physical character of scale producing mineral contaminants so that they flow through piping, heat exchangers, and the like, rather than adhere to the walls thus increasing pressure drop and decreasing heat exchange rate.

SUMMARY OF INVENTION

It is therefore an object of this invention to provide an improved system and method for removing solutes using magnetically conditioned coagulation.

It is a further object of this invention to provide such a system which can reduce the solute level for waste water to be within the requirements set by the Environmental Protection Agency.

It is a further object of this invention to provide such a system which is cost effective to implement.

It is a further object of this invention to provide such a system which requires less

chemical consumption to remove the solutes.

It is a further object of this invention to provide such a system which occupies less space than existing decontamination systems.

5 It is a further object of this invention to provide such a system which can be integrated into existing decontamination systems.

It is a further object of this invention to provide such a system which will improve the performance of existing decontamination systems.

It is a further object of this invention to provide such a system which will cost effectively treat very large flow rates.

10 It is a further object of this invention to provide such a system which uniformly distributes and mixes chemical reagents to maximize their effectiveness.

The invention results from the realization that a truly efficient and cost effective system and method for removing solutes from a fluid can be achieved by magnetically conditioning a fluid by passing the fluid through a high gradient magnetic field before, during or after chemical coagulation and/or the introduction of a nucleation agent to increase both the efficiency and the efficacy of the coagulant by modifying ionic interactions to enhance the formation of colloids.

20 This invention features a method of removing a solute from a fluid using magnetically conditioned coagulation including magnetically conditioning the fluid by applying a conditioning magnetic field to the fluid to enhance the precipitation of solute particles for coagulation, adding a coagulant to the fluid before, during, or after application of the conditioning magnetic field to coagulate the increased available solute particles to form colloids, and collecting the colloids for removal from the fluid.

In a preferred embodiment the conditioning magnetic field may have an average flux density in the range of 0.1 to 6.0 Tesla. The conditioning magnetic field may have a field gradient in the range of 10 to 2000 Tesla/meter. The conditioning magnetic field may be applied parallel to a direction of fluid flow. The step of adding a coagulant may

5 further include nucleation, by adding a nucleation agent, after coagulation. Collecting may include flocculating, by adding flocculant to the coagulated solute particles, to produce flocs. Collecting may include separating the flocs by sedimentation, after flocculation has been completed, to remove the flocs leaving a clear fluid overflow. Collecting may include adding magnetic seed to the coagulated solute particles prior to

10 flocculation. Collecting may include separating the solute particles by sedimentation, after flocculation has been completed, to remove the flocs. Separating may include supplemental magnetic filtration for filtering small flocs from the clear overflow. Collecting may include primary magnetic filtration by applying a primary magnetic field to the flocs, after flocculation has been completed, to remove the flocs from the fluid.

15 The primary magnetic field may have an average flux density of 0.1 to 6.0 Tesla. The primary magnetic field may have a field gradient in the range of 1 to 2000 Tesla/meter. The primary magnetic field may be applied parallel to the direction of a fluid flow. The step of collecting may include mixing at low r.p.m.'s, after adding flocculant, to create large, loose flocs.

20 Collecting may include re-circulating the magnetic seed after removing the flocs from the fluid. Collecting may include shearing the flocs into small pieces. Shearing may include agitating the flocs. Shearing may include shearing the flocs through turbulent fluid flow.

Re-circulating the magnetic seed may include secondary magnetic filtration of the magnetic seed from the flocs by applying a secondary magnetic field to the flocs. The secondary magnetic field may have an average flux density in the range of .1 to 2.0 Tesla. The secondary magnetic field may have a field gradient in the range of 10 to 1000
5 Tesla/meter. The secondary magnetic field may be applied parallel to a direction of fluid flow.

Recirculation may include regeneration of the magnetic seed. Regeneration of the magnetic seed may include demagnetization. Demagnetization may include applying a magnetic field in the range of .1 to 1.0 Tesla at 400 Hertz. Regeneration may include
10 cleaning the surface of the magnetic seed. Cleaning of the magnetic seed may include washing the magnetic seed with acid. Regeneration may include drying the magnetic seed at a high temperature to calcine the seed surface. Drying the magnetic seed may include heating the magnetic seed with microwaves. Recirculating the magnetic seed may include flushing the magnetic seed with water.

15 The fluid may contain less than .1 ppm of solute after collecting the colloids. The coagulant may be alum, ferric chloride, or lime. The percent by volume of alum may be a 48.6% solution and fed in the system at a rate of 10 to 100 ppm.

The flocculant may be anionic or cationic. Mixing may be at low r.p.m.'s for at least 30 seconds.

20 The conditioning magnetic field may have a flux density of at least 0.1 Tesla and a magnetic field gradient of at least 10 Tesla/meter. The nucleation agent may be bentonite, the magnetic seed may be magnetite, the solute may be phosphate and the conditioning magnetic field gradient may be 100 Tesla/meter.

The invention also features a method for removing a solute from a fluid using magnetically conditioned coagulation including applying a conditioning magnetic field to the fluid to enhance the precipitation of solutes for coagulation, coagulating the available contaminants, while contemporaneously applying the conditioning magnetic field to the fluid, to precipitate the solute from the fluid to form colloids, and collecting the colloids.

The invention also features a method for removing a solute from a fluid using magnetically conditioned coagulation including coagulating the solute with a coagulant to precipitate solute particles from the fluid, applying a conditioning magnetic field to the coagulated solute particles to enhance coagulation of the solute particles by increasing application of the solute particles to the coagulant to form colloids, and collecting the colloids.

The invention also features a method for removing a solute from a fluid using magnetically conditioned coagulation including coagulating the solute particles with a coagulant to precipitate the solute particles from the fluid, adding a nucleation agent for receiving the solute particles, and applying a conditioning magnetic field to the coagulated solute particles and nucleation agent to enhance application of the solute particles to the coagulant and deposition of the particles on the nucleation agent.

The invention also features a system for removing a solute from a fluid using magnetically conditioned coagulation including means for magnetically conditioning the fluid by applying a conditioning magnetic field to enhance the precipitation of solute particles for coagulation, means for adding a coagulant to the fluid before, during, or after application of the conditioning magnetic field to coagulate the increased available solute particles to form colloids and means for collecting the colloids from the fluid.

In a preferred embodiment the conditioning magnetic field may have an average flux density in the range of 0.1 to 6.0 Tesla. The conditioning magnetic field may have a field gradient in the range of 10 to 2000 Tesla/meter. The conditioning magnetic field may be applied parallel to the direction of the fluid flow. The means for adding a
5 coagulant may further include nucleation means for adding a nucleation agent. The means for collecting may further include flocculation means, for producing flocs of the available solute particles. The means for collecting may include separator means, responsive to the flocculation means, for separating the flocs from the fluid. The separator means may include sedimentation means in which the flocs settle to the bottom
10 of the sedimentation means and clear fluid overflows the sedimentation means.

The means for collecting may further include seeding means, for adding magnetic seed to the magnetically conditioned fluid. The means for collecting may further include separator means, responsive to the flocculation means, for separating the flocs from the fluid. The separator means may include sedimentation means in which the flocs settle to
15 the bottom of the sedimentation means and clear fluid overflows the sedimentation means. The separator means may further include supplemental magnetic filtration means for filtering small flocs from the fluid overflow. The separator means may include primary magnetic filtration means, responsive to the magnetic seeds, for applying a primary magnetic field to the flocs to separate the flocs from the fluid. The primary
20 magnetic field may have a high field of at least 0.1 Tesla. The primary magnetic field may have a high magnetic field gradient of at least 1 Tesla/meter. The primary magnetic field may be applied parallel to the direction of fluid flow.

The means for collecting may further include seed collection means for collecting the magnetic seed from the separated flocs and recirculating means for recirculating the magnetic seed collected by the seed collection means to the seeding means. The seed collection means may further include shearing means for separating the magnetic seed from the flocs. The recirculating means may include regeneration means for regenerating the magnetic seed. The regeneration means may include demagnetization means for demagnetizing the magnetic seed. The regeneration means may include acidic wash means for cleaning the surface of the magnetic seed. The regeneration means may include drying means. The drying means may include microwave means for applying microwave energy to the magnetic seed to dry the seed.

The primary magnetic filtration means may include a primary magnetic separator. The primary magnetic separator may be a continuous, high gradient magnetic separator, a cyclic high gradient magnetic separator, or a wet-drum type magnetic separator.

The seed collection means may include secondary magnetic filtration means. The secondary magnetic filtration means may include a secondary magnetic separator. The secondary magnetic separator may be a continuous high gradient magnetic separator, a cyclic high gradient magnetic separator, or a wet-drum type magnetic separator. The means for magnetically conditioning may include a filamentary matrix having a length of 6 to 12 inches in the direction of fluid flow. The filamentary matrix may be stainless steel. The stainless steel may be cold worked to induce an austenitic to martensitic phase transformation. The filamentary matrix may be bounded by an iron bound solenoid. The filamentary matrix may be bounded about its periphery by a DC energizing coil for inducing the magnetic field. The filamentary matrix may include an upstream and a

downstream end, the upstream end bounded by a magnetic pole having a plurality of passageways there through and the downstream end may be bounded by a second magnetic pole having a plurality of passageways therethrough, such that a fluid flow is allowed to pass through the first magnetic pole, the upstream end, the downstream end, and the second magnetic pole. The first and second magnetic poles may be oriented to provide a uniform application of the magnetic field to the filamentary matrix.

The flux density of the magnetic field may be in the range of .1 to 6.0 Tesla in a direction normal to the first and second magnetic poles. The magnetic field may have a field gradient in the range of 10 to 2000 Tesla/meter. The filamentary matrix may be bounded at an upstream and by first permanent magnet and at a downstream and by a second permanent magnet, the permanent magnet producing a magnetic field of at least 0.1 Tesla.

The means for magnetically conditioning may include an upstream end and a downstream end and inlet means for uniformly introducing the fluid over the upstream end of the means for magnetically conditioning. The means for magnetically conditioning may include a outlet port for discharging the fluid to a region of non-turbulent flow. The region of non-turbulent flow may provide a retention time of at least 15 seconds to enhance formation of colloids.

The means for magnetically conditioning may further include an upstream end and a downstream end and the means for adding a coagulant may further include introduction means for introducing the coagulant to the fluid. The introduction means may further include distribution means for uniformly distributing the coagulant over the upstream end.

The magnetic seed may be magnetite, the fluid may contain less than .1 ppm of solute after removal of the solute particles, the solute may be phosphate and the fluid may flow at a rate of 10 cm/sec. The primary magnetic separator may include a filamentary matrix and the secondary magnetic separator may include a filamentary matrix.

5 The invention also features a method of removing a solute from a fluid using magnetically conditioned coagulation comprising magnetically conditioning the fluid by applying a conditioning magnetic field to the fluid to enhance the precipitation of solute particles for coagulation, adding a nucleation agent to the fluid before, during, or after application of the conditioning magnetic field to coagulate the increased available solute
10 particles to form colloids, and collecting the colloids for removal from the fluid.

 The invention also features a system for removing a solute from a fluid using magnetically conditioned coagulation comprising means for magnetically conditioning the fluid by applying a conditioning magnetic field to enhance the precipitation of solute particles for coagulation, means for adding a nucleation agent to the fluid before, during,
15 or after application of the conditioning magnetic field to coagulate the increased available solute particles to form colloids, and means for collecting the colloids from the fluid.

DISCLOSURE OF PREFERRED EMBODIMENT

Other objects, features and advantages will occur to those skilled in the art from
20 the following description of a preferred embodiment and the accompanying drawings, in which:

Fig. 1 is a schematic block diagram of a system for removing solutes using magnetically conditioned coagulation according to this invention in which magnetic

conditioning may occur before coagulation, during coagulation, after coagulation or after coagulation and nucleation;

Fig. 1A is a schematic block diagram, similar to Fig. 1, in which coagulation is performed without a coagulant by adding a nucleation agent only;

5 Fig. 2 is a schematic flow diagram, similar to Fig. 1, including the additional collection/removal sub-steps of magnetic seeding, flocculation, separation and removal of the solute and recovery and recycling of the magnetic seed;

Fig. 3 is a detailed schematic flow diagram, similar to Fig. 1, of a system according to this invention in which magnetic conditioning occurs before coagulation and
10 the solutes are separated for collection and removal by flocculation and sedimentation without magnetic seeding;

Fig. 4 is a detailed schematic flow diagram, similar to Fig. 2, in which the solutes are separated for collection and removal by magnetic filtration followed by magnetic separation of the magnetic seed from the sludge, recycling of the seed, and regeneration
15 of the seed surface;

Fig. 5 is a detailed schematic flow diagram, similar to Fig. 2, in which the solutes are separated for collection and removal by sedimentation followed by magnetic separation of the magnetic seed from the sludge, recycling of the seed and regeneration of the seed surface;

20 Fig. 6 is a schematic cross-sectional view of the magnetic conditioner oriented transverse to the direction of the magnetic field and the fluid flow; and

Fig. 7 is an elevational view showing the reagent inlet and flow distribution piping of the magnetic conditioner of Fig 6.

Although specific features of this invention are shown in some drawings and not others, this is for convenience only as each feature may be combined with any or all of the other features in accordance with the invention.

5 The system for removing solutes from a fluid using magnetically conditioned coagulation is shown generally as reference numeral 10, Fig. 1. In a preferred embodiment, a fluid, for example waste water effluent from a sewage treatment plant after sludge sediment removal, undergoes magnetic conditioning 12 by applying a high magnetic field parallel to the fluid flow, the fluid flow having a velocity of at least 3 cm/sec. After magnetic conditioning 12 the fluid undergoes coagulation 14 to precipitate
10 the contaminant, e.g. phosphate, from the fluid to form colloids. It has been found that magnetic conditioning of the fluid allows the solute, in this case a contaminant such as phosphate, to become more readily available for coagulation, allowing the coagulant to become more efficient. The result is that much smaller quantities of coagulant are required than in previous purification systems, yet more contaminant, e.g. phosphate,
15 precipitates from the fluid. However, the present invention may be used to remove valuable solutes to be utilized in various applications, and is in no way limited to phosphate removal from waste water.

After coagulation 14 of the solute, the precipitated solute particles, colloids, undergo collection 16. Once collection of the colloids is complete, the fluid is discharged
20 20 with a solute level of less than 0.05 parts per million (ppm). The decontaminated fluid may undergo further processing including disinfection 22 if necessary to remove bacteria from the fluid.

While in the embodiment in Fig. 1 system 10 performs magnetic conditioning 12 prior to coagulation 14, magnetic conditioning may also occur contemporaneously with coagulation, magnetic conditioning 12', after coagulation, magnetic conditioning 12'', or after coagulation 14 which includes nucleation 18, magnetic conditioning 12''', all shown in phantom, to enhance precipitation and attachment of the solute to the coagulant and/or the nucleation agent. The various embodiments have been shown in phantom in order to reduce the number of drawings. However, one skilled in the art will realize that magnetic conditioning need only take place either before, during or after coagulation where coagulation may be defined as including or not including nucleation. The dramatic improvement using the magnetic conditioning taught by this invention is due to the effect of the magnetic field on ionic interactions of the solute which modifies the hydration of the ions, creating favorable conditions for the formation of new ionic associates which enhance the formation of colloids.

Magnetic conditioning also changes the internal energy of the system which further influences intermolecular interactions. The magnetic field influences the surface forces of the colloids causing the magnetic dipoles to align, thus creating forces which further enhance the growth of the colloidal particles.

The Lorentz VXB forces on the moving electrical charges also tend to align the electric dipoles. This alignment of previously randomly oriented dipoles enhances the regrouping of existing ionic associates which enhances the formation of colloids. Coagulation enhancement is thus influenced by the magnitude of the magnetic field, the gradient of the magnetic field, the orientation of the magnetic field with respect to the

direction of the fluid flow and the velocity of the fluid flow in the region of the magnetic field.

Although the preferred location of the magnetic conditioning means is prior to coagulation and the preferred orientation of the magnetic field is parallel to the direction of the fluid flow, the effects described herein will occur independent of its location in the flow treatment system or the orientation of its field with respect to the fluid flow.

In a preferred embodiment it is also a purpose of the magnetic conditioning means to create local turbulent mixing to reduce the equivalent mean free path of magnetically modified ionic species to enhance the creation of new associates. In the presence of the means for introducing such turbulent mixing, the parallel flow creates a combination of magnetic and hydrodynamic conditions which favor the electrochemical interaction which initiates nucleation of the colloid.

For the process variation wherein the coagulant is introduced ahead of, or in, the region of magnetic field, it is also important to create adequate turbulence to assure intimate mixing of the reagent throughout the body of the fluid.

For optimum performance the magnetically conditioned coagulation should be followed by a region of more quiescent, non-turbulent flow to provide time for the formation and growth of colloids.

Although the effect of the preconditioning disappears with time (up to one hour) it is maximized with a retention time of up to ten minutes between the preconditioning and addition of the chemical coagulant. In the case of contemporaneous magnetic conditioning and coagulation, the retention time is up to two minutes after coagulation.

In yet another embodiment, it has been found that a coagulant is not always necessary. After magnetic conditioning 12, Fig. 1A, coagulation is enhanced by nucleation 18a which is performed with the addition of a nucleation agent. Once nucleation 18a is complete, the coagulated particles are collected and removed 16.

5 However, as shown above with reference to Fig. 1, magnetic conditioning may also take place contemporaneously with nucleation, magnetic conditioning 12', or after nucleation, magnetic conditioning 12'', both shown in phantom.

10 In summary, system 10 may comprise several embodiments by incorporating magnetic conditioning before, during, or after coagulation 14 or after coagulation 14 and nucleation 18, prior to collection and removal 16 of the solute, or before, during, or after nucleation 18a, prior to collection and removal 16. While system 10 may be used to remove various solutes, it has been found extremely effective in removing phosphates from sewage effluent. By magnetically conditioning waste water effluent, it has been found that phosphate levels of the discharged fluid may be reduced to less than .025 ppm, 15 well below the proposed EPA requirement of .1 ppm required to control eutrophication.

20 In a preferred embodiment, magnetic conditioning 12 includes magnetic preconditioning means 24, Fig. 2, which applies a high magnetic field having an average flux density of 0.1 to 6.0 Tesla and a field gradient of 10 to 2000 Tesla/meter. The magnetic field is applied parallel to the flow of the fluid which is indicated by arrow 21. After magnetic preconditioning 12 of the fluid, the fluid undergoes coagulation 14 by adding a coagulant 26 such as alum, ferric chloride, lime, or any other suitable coagulant to the magnetically conditioned fluid. Alternatively, all or a portion of the coagulant can

be introduced contemporaneously 26' directly into the magnetic preconditioning means 24.

Coagulation 14 may include nucleation 18 in addition to coagulation. Nucleation 18 may be performed contemporaneously with coagulation 14. A nucleation agent 28, such as bentonite available through American Colloid Co., Arlington Heights, IL, is added to the magnetically conditioned solution. The addition of a nucleation agent to the magnetically conditioned and coagulated fluid provides additional sites for deposition of the phosphate, thus allowing greater precipitation of the solute from the waste water to increase the amount of phosphate removed from the fluid.

Once nucleation has been completed, the solute, for example phosphate, undergoes collection and removal 16. The magnetically conditioned slurry of fluid, treated with alum and bentonite, undergoes magnetic seeding 30 in which a magnetic seed 32, such as magnetite which is a natural ore such as that produced by Northshore Mining Co., Silver Bay, MN, is added to aid in the separation of the phosphate.

However, this is not a necessary limitation as any other magnetic material may be used as magnetic seed. Magnetite is chosen because its amphoteric surface provides natural and highly effective scavenging of microbiological contaminants such as coliform bacteria, viruses and other micron-sized pathogens such as cryptosporidium parvum and giardia lamblia thereby requiring less disinfectant. Once magnetic seeding 30 is complete, the magnetically conditioned slurry undergoes flocculation 33 in which flocculant 34 is added to form loose flocs containing coagulated phosphate, nucleation agent 28, magnetic seed 32 and any remaining suspended solids present in the fluid being treated. One such flocculant is Percol 737, manufactured by Allied Collids, Suffolk, VA or, Magnifloc,

manufactured by Cytec Industries, of West Paterson, NJ. Flocculant 34 may be anionic or cationic, depending on the nature of coagulant 26 and the pH of the effluent.

After flocculation 33 the flocs are removed from the fluid by separator 36. Once separation has been completed, magnetic seed 32 is separated from the flocs and
5 recirculated to magnetic seeding 30.

Alternatively, magnetic conditioning 12, Fig. 3, coagulation 14 and nucleation 18, may occur to enhance collection and removal 16 of solute particles as discussed above, however, flocculation 33 occurs without magnetic seeding and separation 36 takes place through sedimentation. Flocculation 33 creates loose flocs. Separation 36 through
10 sedimentation is achieved by allowing adequate time for the flocs to settle to the bottom of the settling tank 108. The phosphate-containing sludge is removed from the bottom of tank 108 for further processing and disposal while clean water flows from the top of the settling tank for further processing such as disinfection and storage.

Magnetic conditioning 12, Fig. 4, includes magnetic conditioning means 24 which
15 may include a magnetic conditioner. Magnetic conditioning means 24 applies magnetic field 38, having a magnetic gradient of at least 10 Tesla per meter parallel to the direction of fluid flow 21. In a preferred embodiment the best results are obtained with a magnetic field gradient of at least 100 Tesla per meter. The magnetically conditioned effluent is fed into coagulation means 14' which include coagulation tank 40. Coagulant 26 is also
20 fed into coagulation tank 40 by coagulation pump means 42. Coagulant 26 may be fed at a rate of 10-100 ppm. Where the contaminant is phosphate, coagulant 26, such as alum, is added to obtain a ratio of 10-100 ppm, or 48.6% solution by volume, depending on the initial phosphate content and the desired reduction level. Coagulation mixing means 44

intensely mixes coagulant 26 with the magnetically conditioned effluent. The intense mixing should last for at least 3 minutes in order to obtain complete mixing of coagulant 26 with the effluent.

Coagulation means 14' may also include nucleation means 18', which includes nucleation tank 46. The slurry containing the magnetically conditioned effluent and coagulant 26 is fed from coagulation tank 40 into nucleation tank 46. Nucleation agent 28 is fed into nucleation tank 46 by nucleation pump means 48 at a rate of 25-100 ppm. Nucleation mixing means 50 mixes the slurry and nucleation agent 28. In a preferred embodiment, the mixing lasts at least 3 minutes, however, the mixing need not be as intense as coagulation mixing means 44.

The slurry containing the magnetically conditioned fluid, coagulant 26 and nucleation agent 28 is then fed into magnetic seeding means 30', of collection and removal means 16', which includes seeding tank 52. Magnetic seed 32, such as coarse magnetite, is fed into seeding tank 52 by seeding pump means 54. Good results are obtained when magnetic seed 32 is added at a rate of 2,000-5,000 ppm. Seed mixing means 56 mixes the slurry and magnetic seed 32 thoroughly. Typically the mixing time is at least 1 minute. It has also been found that by adding large amounts of magnetic seed 32, the mixing time may be reduced. In order to ensure thorough, complete mixing, the mixing can be done in the respective tanks. However, this is not a limitation to the invention. Mixing may also be accomplished by static in-line mixers which would replace the tanks and mixing means shown in the figure, or both.

The slurry now containing the magnetically conditioned fluid, coagulant 26, nucleation agent 28 and magnetic seed 32 is fed into flocculation tank 58 where

flocculant 34 is added by flocculation pump means 60 at a rate of .5-2.0 ppm.

In order to create large loose flocs 64 from which the magnetic seed can be more easily separated for recycling, flocculation mixing means 62 mixes the slurry at low r.p.m.'s so that the flocs will not be sheared apart. Good results are obtained with
5 flocculation mixing times of at least 30 seconds but no more than 3 minutes.

After flocculation 33' is complete the slurry, comprised of clean water and flocs 64, is pumped into separator 36' by separator pump means 66. Separator pump means 66 includes a positive displacement pump such as a piston and diaphragm or a screw type pump in order to avoid shearing apart flocs 64. Separator 36' may include primary
10 magnetic filtration means 68 and may be a continuous high gradient, cyclic high gradient or wet-drum type magnetic separator. Primary magnetic filtration means 68 applies a high magnetic field having an average flux density of .1 to 6.0 Tesla and a field gradient from 1 to 2000 Tesla/meter, characterized by magnetic field lines 70, to the slurry to remove from the effluent flocs 64, which contain magnetic seed 32, coagulant 26,
15 nucleation agent 28, entrapped phosphate and other suspended solids. The magnetic field is preferably applied parallel to the direction of fluid flow. The clear water is removed from separator 36' by discharge pump means 72.

Magnetic seed 32 collected by primary magnetic filtration means 68 may be flushed from primary magnetic filtration means 68 by using clean water from discharge
20 pump means 72, or using raw water which has already been treated with coagulant 26 and nucleation agent 28 from nucleation pump means 45.

The separated flocs 64 are collected in collection tank 75 and then pumped from separator 36' by removal pump 74 back into seeding tank 52. The solute (phosphate)

loaded seed can be recycled up to ten times, after which the separated flocs 64 are eventually collected in collection tank 75 and pumped by removal pump 74 into shearing tank 76 of seed collection means 83. Shearing tank 76 includes shearing means 80 which shear the flocs into small pieces. Shearing means 80 may include agitating the flocs to produce small pieces. The sheared flocs are then fed to secondary magnetic filtration means 78, which may include secondary magnetic separator 82, (e.g. a continuous high gradient, cyclic high gradient, or wet-drum type magnetic separator), by shearing pump 77. Alternatively, flocs may be sheared into small pieces by turbulent flow through secondary magnetic separator 82.

In the event that the secondary magnetic separator 82 is a high gradient magnetic separator, shearing of the flocs may be accomplished by turbulent flow within the matrix of secondary magnetic separator 82.

Secondary magnetic filtration means 78 applies a high magnetic field with a flux density in the range of 0.1 to 2.0 Tesla and a field gradient of 1 to 1000 Tesla/meter to the sheared flocs to separate magnetic seed 32 from the sheared flocs. The recovered magnetic seed 32 is collected by seed collector 84 which includes seed collection tank 86. The collected magnetic seed 32 is then recirculated by recirculation means 88, which includes recirculation pump 90, which returns the magnetic seed 32 to magnetic seeding means 30'.

The sheared flocs from which the magnetic seed 32 has been removed, are collected by sludge collection tank 92 and are then pumped to sludge filter 94 by sludge pump means 96. Water is removed from the sludge by sludge filter 94 and may be returned to coagulation tank 40. The sludge may be further treated by additional means

such as biological activation typical of waste water treatment facilities and well known to those skilled in the art.

5 Magnetic seed 32 collected by secondary magnetic filtration means 78 may be flushed from secondary magnetic separation means 78 by using clean water from discharge means 72.

By recirculating magnetic seed 32, the amount of flocculant 34 required may be reduced. Further, less magnetic seed 32 is required and thus less space is required to maintain magnetic seed 32. Thus, regenerating magnetic seed decreases operation costs.

10 Regeneration of seed 32 may be accomplished by diverting all or a portion of the recycled seed discharged from recirculation pump 90 through seed regeneration means 101. Regeneration means 101 may include seed demagnetization means 102, seed surface cleaning means 103, and seed drying means 104, any or all of which may be used independently or in any combination. Seed demagnetizing 102 is accomplished by passing the seed through an alternating magnetic field of 0.1 to 1.0 Tesla and 400 Hertz.

15 Seed surface cleaning means 103 may include acidic chemical cleaning such as acetic, chlorhidric, or sulfuric acid washing. Drying means 104 may include microwave heating, or convection oven heating, preferably in an oxygen-free environment. The seed is dried at a very high temperature to calcine the seed surface, but below the melting point or fusing point of the seed.

20 In another embodiment, magnetic preconditioning means 12, Fig. 5, coagulation means 14', nucleation means 18', magnetic seeding means 30' and flocculation means 33' are the same as discussed above with reference to Fig. 4. However, separator means 36'' includes sedimentation means 106, similar to that discussed in Fig. 3, instead of magnetic

filtration. Separator pump means 66' feeds flocs 64' into sedimentation means 106 which may include settling tank 108. Magnetic seed 32' accelerates the settling velocities of flocs 64' in settling tank 108. Typical settling velocities are enhanced to greater than 0.5 cm/sec, dramatically decreasing the time it takes for flocs 64' to settle.

5 Provided that flocculation 33' has formed large, loose flocs 64', the overflow of sedimentation means 106 is a clear fluid which overflows settling tank 108 into supplemental magnetic filtration means 110 which magnetically separates smaller flocs that may have been created by disturbances in the flow of flocs 64' into settling tank 108 from separator pump means 66' and, because of their small size, did not settle in
10 sedimentation means 106.

 Supplemental magnetic filtration means 110, similar to primary magnetic filtration means 68, and secondary magnetic filtration means 78, Fig. 4, applies a high magnetic field, represented by magnetic field lines 112, of at least 0.1 Tesla and a magnetic field gradient of at least 10 Tesla/meter. In a preferred embodiment the
15 magnetic field gradient is at least 100 Tesla/meter. The slurry collected in settling tank 108 of sedimentation means 106 is then processed in a manner similar to that of Fig. 4.

Flocs 64' are collected and fed by removal pump means 72' to secondary magnetic filtration means 78' which includes secondary magnetic separator 82'. Magnetic seed 32' is collected by seed collector means 84' and recirculated by recirculation means 88'.

20 Recirculation means 88' includes recirculation pump 90' which recirculates the collected magnetic seed 32' to magnetic seeding means 30'. The recirculated magnetic seed may be recirculated directly into the magnetically conditioned, coagulated fluid, or it may be

added to magnetic seed 32'.

Periodic seed regeneration means 101' including seed demagnetization means 102', seed surface cleaning means 103', and seed drying means 104' are the same as discussed above with reference to Fig. 4. Magnetic conditioning 12, may include
5 magnetic conditioning means 24 and coagulant feed means 26', Fig. 3.

Magnetic conditioning means 24, which can be circular or rectangular in cross section, Fig. 6, provides a magnetizing field indicated by arrow 124 throughout a working volume occupied by ferromagnetic, filamentary matrix 122 having a length of 6-12 inches in the direction of fluid flow 136. The field strength should be in the range of 0.1 to 6.0
10 Tesla which may be derived from either conventional or superconducting coil windings or permanent magnets. Magnetic conditioning means 24 may include an iron bound solenoid comprised of DC energizing coil 128 surrounded by a low carbon steel magnetic frame comprised of a flux return portion 132 and magnetic pole plates 134 arrayed and supported on either surface of ferromagnetic filamentary matrix 122 for producing the
15 magnetic field. Field strengths in excess of 6.0 Tesla can be derived with the use of super-conducting energizing coil windings. Magnetic flux in the range of 0.1 to 6.0 Tesla is induced throughout the entire volume bounded by coil 128 and pole plates 134 in a direction indicated by arrow 124, normal to the internal pole surfaces. Magnetic field 124 magnetizes the matrix filaments transverse to their long dimension, thereby creating very
20 high magnetic field gradients at the filament edges which are aligned with magnetizing field 124. Ferromagnetic filamentary matrix 122 includes layered stainless steel wool or expanded metal, each of which is characterized by very sharp edges which help to create very high magnetic field gradients.

Fluid to be treated indicated by arrow 136 is introduced to the upstream surface of magnetic conditioning means 24 via primary flow inlet duct 138. Fluid 136 flows through slots 140 between upstream pole plates 134, through magnetized filamentary matrix 122, between slots 140' and downstream pole plates 134' and discharging into primary flow discharge duct 142. The length of primary flow discharge duct 142 is selected to provide a retention time of thirty seconds to two minutes of non-turbulent flow to enhance formation of colloids.

The magnitude of the gradient of a magnetic field is inversely proportional to the physical size of the magnetized element that creates it, and the depth or distance that the field strength extends from the surface of that element is proportional to the physical size of the element. The most efficient means of producing a uniform field within the magnetic conditioning working volume is with an iron bound solenoid comprised of energizing coil 128 bound by iron flux return 132 and iron pole plates 134. Very high local magnetic field gradients are produced at thousands of sites distributed throughout the working volume by positioning a matrix consisting of a very large number of fine ferromagnetic filaments in the field. The average diameter of such filaments is typically less than 0.5 mm. The filaments are positioned such that they are generally transverse to the direction of the magnetizing field. When fully magnetized, a filament of this size can create a magnetic field gradient of up to 2000 Tesla/meter. Accordingly, the magnitude of the magnetic field anywhere in the working volume can never be less than that of the magnetizing field.

While filamentary matrix 122 is typically constructed from stainless steel wool or expanded metal, other construction techniques and materials will be obvious to one

skilled in the art. The preferred use of corrosion resistant, 300 series, stainless steel requires that the matrix manufacturing process introduce adequate cold work into the metal to cause a transition from the austenitic, paramagnetic phase of normal 300 series stainless steel to a martensitic, ferromagnetic phase. Other matrix materials may be used
5 such as 400 series stainless steel which is normally ferromagnetic or nickel which is useful in highly corrosive chemical applications.

Placing the ferromagnetic filament matrix 122 within the magnetic field according to the present invention is unique to the magnetic field conditioning application and represents a far more efficient and much lower cost design than that of the prior art. This
10 will be particularly true for large flow volume applications wherein their use will result in significant reductions in both the size and cost of new system installations. Although the background field for most practical application will be in the range of 0.1 to 2.0 Tesla there may be application which can take advantage of fields as high as 6.0 Tesla which are realistically available with the use of superconducting energizing coils. Alternatively,
15 the magnetic field may be provided by permanent magnets.

It has been found that by providing coagulant introduction and distribution plumbing at the inlet surface of the magnetic conditioning system, the combined magnetic and hydraulic design features allow cost effective treatment of very large flow rate systems and also provide uniformly distributed introduction and thorough mixing of
20 chemical reagents into the flow stream of the water to be treated. The device can thus eliminate the need for costly reagent flash-mixers.

For contemporaneous magnetic conditioning 12' and coagulation 14, as discussed with reference to Fig. 1, magnetic conditioning means 24, Fig. 6, includes coagulant flow

distribution inlet manifold 144 and coagulant flow distribution piping 146. Coagulant 26' flows through input manifold 144 and into distribution piping 146 which discharges coagulant 26' into slots 140 by means of holes 148, Fig. 7, arrayed along the full length of flow distribution piping 146 proximate said slots. Thus, coagulant 26 is thoroughly dispersed throughout primary fluid stream 136 by turbulent mixing induced by matrix 122.

Magnetic conditioning means 24 according to this invention may accommodate a flow rate of 5 million gallons per day, providing 2500 square inches of matrix flow cross sectional area. However, other means for providing distributed flow through the poles of the magnet and for introduction and distribution of chemical reagents or other filter aids into the primary flow streams are possible within the context of this invention.

Other embodiments will occur to those skilled in the art and are within the following claims:

What is claimed is: